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#### **TECHNICAL REPORT NO.5**

# Growth on the Reconstructed Diamond (100) Surface

by

S. J. Harris and D. G. Goodwin

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### Growth on the Reconstructed Diamond (100) Surface

by

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#### **Abstract**

A thermochemical kinetics analysis has been carried out for growth on the (100)-(2×1):H diamond surface using a pair of previously proposed mechanisms which operate sequentially. Half of the growth on such a surface is accounted for by insertion into dimer bonds, while the other half is accounted for by addition across troughs between dimer bonds. The latter mechanism is slower and therefore controls the overall growth rate on this surface. This result can explain the success that the latter mechanism has had in predicting growth rates in a variety of systems. We suggest that growth at step sites is favored on steric and thermochemical grounds and can account for atomically smooth surfaces on diamond.

#### Introduction

In the past few years several detailed growth mechanisms have been proposed to explain the chemical vapor deposition (CVD) of diamond films [1–10]. In general, these models have used the formal resemblance between the bonding and structure in diamond and in alkanes to postulate [6] that chemistry on the diamond surface could be understood in terms of the very well known chemistry of alkanes. In effect, the assumption is made that the chemistry of a diamond surface is controlled by the local electronic environment, as is true for alkanes, and that bulk band structure and surface states play no role. If this postulate is valid, then considering all that is known about alkane chemistry, we may be able to understand CVD diamond growth at a level of detail beyond that for any other CVD process.

Considerable research in the field has been aimed at determining the "growth" species, i.e., the gas phase species directly responsible for diamond formation [11, 12], and recent experiments have demonstrated that the  $CH_3$  radical is the primary growth species in the CVD systems that have been examined [13–19]. One proposed chemical kinetics mechanism [2], which takes  $CH_3$  as the growth species, successfully predicts [20–22], experimental growth rates for both RF [21] and DC [23] plasma torches, for flames at low and atmospheric pressure [15, 24, 25], and for filament systems as a function of pressure and composition [16, 17], without the use of adjustable parameters. Its predictions are compared to experiment in Figure 1. The ability of the model to predict the relative growth rates for these very different systems is striking. However, we have pointed out [2] that the near-perfect absolute agreement is fortuitous—our estimated uncertainty is a couple of orders of magnitude in either direction [2]. This is because there is uncertainty not only in gas phase rate and thermodynamic parameters themselves, but also in how these parameters should be converted for use with surface kinetics. As discussed previously [2], the mechanism

models the diamond surface with the 9-carbon molecule bicyclononane (BCN), which in effect takes the diamond surface to be an unreconstructed (100) surface. However, it is unlikely that such a surface would be stable because of very large H – H steric repulsions [26]. Recent STM and AFM experiments have shown [27-29] that diamond surfaces can be rather rough on an atomic scale, but at least some of the surface reconstructs to the (100)-(2×1):H form [28, 30, 31]. On this surface each carbon atom is bonded twice to carbons in the bulk, once to a surface hydrogen, and once to a neighboring surface carbon making a "dimer" and forming a 5-membered ring, as seen in Figure 2. A quantitative analysis of the steric forces on various (100) surfaces shows that this dimer reconstruction substantially reduces surface stress compared to the unreconstructed surface [26, 32]. In this paper we propose that the growth kinetics on the (100)- $(2\times1)$ :H surface can be understood by combining two different mechanisms—a "trough" mechanism (identical to the BCN mechanism) and a "dimer" mechanism—which operate sequentially on the two types of sites present on this surface. This picture of growth can explain the success that the BCN mechanism has enjoyed.

#### **Analysis**

Any acceptable diamond growth mechanism must be both fast enough to explain observed growth rates and thermodynamically favorable enough so that the overall reaction in the reverse direction (etching) is negligible [2, 33, 34]. The latter requirement comes from the experimental observation that etching by atomic hydrogen is extremely slow. In this section we describe our analysis for the thermochemistry and kinetics of proposed growth mechanisms which satisfy these conditions.

#### Structure of the Model Compound

The first step is to choose a model structure to represent the diamond crystal and surface. Use of very large model structures is a requirement if steric energies—which can be quite large—are to be calculated accurately. This is because the calculation must take into account the fact that lattice atoms close to a surface reaction site may move somewhat to relieve steric repulsions, but it must also take into account that the crystal as a whole is extremely rigid. For estimating steric energies, we used the crystal slab shown in Figure 2, which is 1.6 by 1.6 by 0.6 nm (8 layers) thick and contains 330 carbon atoms and 20 surface dimer bonds. Reaction takes place near the center of the slab. Although this crystal is relatively large, when finding the steric energy it was necessary to hold twenty atoms at the base and edges of the crystal fixed in order to prevent the crystal from flexing due to the large surface tensile stress induced by the dimers. For estimating heat capacities and entropies we used a smaller (160 carbon atoms) 1.0 by 0.6 by 0.6 nm thick diamond slab because of limitations of the computer program.

## Gas Phase Species Concentrations

For the models discussed here we assume that growth occurs from reaction of the  $CH_3$  radical at the diamond surface. We take gas phase concentrations from measurements and modeling [12, 35-37]. For our typical filament-assisted growth conditions with the substrate temperature 1200 K and the pressure 20 torr we have  $X_H = 2 \times 10^{-3}$  and  $X_{CH_3} = 2 \times 10^{-4}$ , where  $X_i$  is the mole fraction of species i.

#### Rate Constants

Rate constants for the gas-surface reactions that appear in these mechanisms have not been measured. In order to estimate their values we have made the assumption [4] that the reaction cross section per surface site is equal to the reaction cross section per equivalent site in a prototype gas phase reaction. According to our analysis for

an abstraction by a gas phase species of mass  $m_g$  this assumption leads to [4]

$$k_s = k_g n_s [\mu/m_g]^{1/2},$$

where  $k_s$  and  $k_g$  are the surface and gas phase rate constants, respectively,  $\mu$  is the reduced mass of the reactants in the prototype gas phase reaction, and the symmetry number  $n_s$  is the number of identical sites on the surface structure being examined. In other words, the surface rate constant equals the gas phase rate constant corrected for the effect of collision frequency and for symmetry. We use the same approach for radical recombination reactions, with one difference. We consider the radical site on the gas phase molecule to be equivalent to two surface radical sites because the nearly-planar gas phase radical has two equally probable sides for reaction, whereas the surface radical has only 1 side from which reaction can occur. Thus, for radical recombination we have

$$k_s = 0.5 \, n_s k_g [\mu/m_g]^{1/2}$$
.

Assuming a constant reaction cross section neglects some factors which may affect the surface rate constant. Steric hindrances and reaction barriers might differ on the surface from those of the prototype gas phase reactions. Also, transition state theory shows that the pre-exponential factor is determined by the entropy change  $\Delta S^{\ddagger}$  in forming the activated complex; even if the reaction potential surface is the same for the prototype and surface reactions, differences in the translational and rotational contributions to  $\Delta S^{\ddagger}$  may alter the pre-exponential factor somewhat. These effects are ignored here, since they are difficult to estimate accurately and are not expected to qualitatively affect our conclusions.

The rate constants are shown in Tables 1 and 2. (Definitions of the species are given below.) Two surface isomerization reactions in Table 1, G and H, are treated differently. We do not expect a significant barrier for Reactions G, so we have assigned it a large rate constant which simply insures that this reaction is in partial equilibrium.

The rate constant for Reaction H has been estimated by Musgrave, Goddard, and Harris [38] using ab initio quantum techniques.

#### Thermochemistry

We estimate values for the enthalpy change  $\Delta H$  and entropy change  $\Delta S$  in order to determine  $\Delta G = \Delta H - T\Delta S$  for each reaction. From  $\Delta G$  we can calculate rate constants for reverse reactions, which are related to the forward rate constants by

$$K_{eq} = k_f/k_r = e^{-\Delta G/RT},$$

where  $K_{eq}$  is the equilibrium constant. (Thermochemical quantities are tabulated for standard states of 1 atmosphere, whereas we are using concentration units. For reactions in which the number of moles changes,  $k_r$  must be multiplied by a factor which converts between atmospheres and moles/cm<sup>3</sup>.)

To estimate thermodynamic parameters we have suggested the use of molecular mechanics [34]. With this technique, a force field is established that describes the interaction of every atom in the system with every other atom. In general, both the functional forms for the interactions and the associated coefficients are chosen empirically. A number of force fields have been proposed for carbon atoms [39–41], but the most widely used and extensively tested force fields for obtaining thermodynamic quantities are MM2 [42] and MM3 [43], which we use in this paper. These force fields, which were designed specifically to estimate steric repulsions in highly strained alkanes, give each bond a set of force constants (e.g., stretching, bending, torsion) for displacement from "natural" lengths and angles, and give each atom van der Waals attractions and repulsions to the other atoms in the system. Our codes use the MM2 or MM3 force fields to adjust the position of every atom in the system in order to minimize the total strain energy  $E_{strain}$ , which is the result of bonds bending, stretching, and twisting in response to van der Waals attractions and repulsions. The heat of formation  $H_f$  for a molecule is obtained by combining this calculated  $E_{strain}$ 

with bond enthalpies  $H_{bond}$  calculated from an associated group additivity scheme. MM2 and MM3 predict  $H_f$  of even very crowded and highly strained molecules to within typically 0.5 kcal/mole (0.02 eV/molecule), which is not much greater than the experimental error [42, 43]. On the other hand, since MM3 is a purely empirical force field and has not been calibrated against a diamond surface, we do not expect the predicted energetics to be so accurate for the present work. For example, we estimate that fixing atoms at the base and edges of the model compound (see above) introduces an uncertainty of around 1 or 2 kcal/mole in relative heats of formation. (Only relative—not absolute—heats of formation appear in the analysis.) The MM3 force field can also calculate vibrational frequencies. For stable structures we use the enthalpy calculations from MM3. Since the radical force field in that code has not yet been finalized [44], we use the MM2 force field to estimate the difference in the heats of formation of stable species and radical species with a hydrogen removed. Heats of formation calculated by MM2 and MM3 differ significantly only where there are non-bonded H-H distances less than 0.2 nm [43], which occur for the species  $C_5M$ and  $C_6HM$ . For these cases, an error of 1 to 2 kcal/mole may be introduced by our use of MM2. The entropy is calculated primarily by using the MM3 code. However, we have also included a symmetry term  $-R \ln n_s$  to take into account the presence of identical atoms for some of the surface structures, and we treat  $-CH_3$  and  $-CH_2^*$ groups as free rotors. Treating these as free rotors is a good approximation, since the barriers to rotation are found to be typically less than 1 kcal/mole. Thermodynamic quantities calculated at 1200 K for the two mechanisms considered, relative to the  $C_5$ starting structure (see below), are shown in Table 3 and 4.

#### Reaction Mechanisms

Carbon atoms can add onto the (100)- $(2\times1)$ :H surface at two types of sites, inserting into dimer bonds or adding across troughs between dimer bonds. To complete

a new monolayer, half of the carbons must add to the dimer sites and half to the trough sites. The added carbons may then dimerize with their neighbors, forming a new (2x1) surface on a new layer, with dimer rows orthogonal to the original rows. Recently, Garrison and co-workers [45] have proposed a mechanism for insertion into dimer bonds which involves exclusively reactions that have low activation barriers and well-known analogs in hydrocarbon chemistry. (Another proposed mechanism for insertion into dimer bonds [46] includes a step with a 3-center transition state. Since the barrier at that transition state is calculated [46] to be very high, it is not considered further.) For addition across the troughs we use the bicyclononane (BCN) mechanism, which was originally proposed [2] to explain growth on the unreconstructed (100) surface. Although the atoms making up a trough are isomorphic to those on an unreconstructed (100) surface, on the (100)-(2×1):H surface the strain energy associated with this structure is substantially reduced. Thus, the BCN mechanism can be applied more realistically to troughs on the (100)-(2×1):H surface.

#### Dimer mechanism

The steps in the dimer mechanism of Garrison et al. [45] are reviewed in Table 1. This mechanism begins with the dimer structure on the (100)-(2×1):H surface, which we denote  $C_5$  (Figure 3a) because of the presence of 5-membered rings. In the initial step (Reaction A) a surface hydrogen is abstracted by a gas phase H atom forming the tertiary surface radical  $C_5^*$  and the  $H_2^{gas}$  molecule. Either  $H^{gas}$  (Reaction B) or  $CH_3^{gas}$  (Reaction C) can recombine at this radical site to give  $C_5$  or  $C_5M$ , respectively. A hydrogen atom from the methyl group of  $C_5M$  can be abstracted to give  $C_5M^*$  (Reaction D), which in turn may react with  $H^{gas}$  (Reactions E or F). In the next step (Reaction G)  $C_5M^*$  isomerizes to  $C_d^*$  (Figure 3b), a species which contains both a radical site and a double bond. Reaction G is called a  $\beta$  scission reaction [47] because the C-C bond two carbons away (or " $\beta$ ") from the radical site is broken during this isomerization reaction. (Two other C-C bonds can also break via a  $\beta$ 

scission reaction; products of those reactions are not considered here.) The radical carbon in  $C_d^*$  can react with either end of the carbon-carbon double bond. Addition to the end closest to the bulk diamond reverses Reaction G, while addition to the other end forms the  $C_6^*$  species (Reaction H, Figure 3c). Finally,  $C_6^*$  and  $C_6$  interconvert by Reactions I and J. We note that a total of two hydrogen abstraction reactions are necessary to form  $C_6$  from  $C_5$ .

#### Trough Mechanism

The steps involved in adding carbon across the trough on the (100)- $(2\times1)$ :H surface are identical to those proposed previously in the trough mechanism [2, 3] (except that formation of long-chain hydrocarbons, Reaction j, is not considered here), and they are shown in Table 2. Briefly, a methyl radical adds at a radical site formed from abstraction of one or both of the trough hydrogens (see Figure 3e). This step is followed either by abstraction of the other trough hydrogen and one of the methyl hydrogens (Reactions d or f and k after Reaction c) or by abstraction of a methyl hydrogen (Reaction l after Reaction s) to give the  $C_6B$  structure, which has a carbon atom that bridges the trough. For reasons discussed below, we allow the trough mechanism to occur only adjacent to  $C_6$ -type sites just formed by the dimer mechanism, as shown in Figure 3e. Thus, the starting structure is called  $C_6HH$ , which refers to the two H atoms pointing toward each other across the trough and next to a newly-formed  $C_6$  species. The final bridged structure is called  $C_6B$ . We note that a total of three hydrogen abstraction reactions are necessary.

#### Results

#### Dimer mechanism

The time dependence for the dimer mechanism is calculated by integrating the rate equations for Reactions A through J. Initially, the fraction of the dimer sites which are  $C_5$  is 1.0, and the fraction of all other species in the mechanism is 0. The

calculation shows the surface rapidly reaches steady state, within less than 100 ms. However, there are no irreversible steps in this mechanism, since those steps which have a large enthalpy reduction also have a substantial reduction in entropy. The result is that the reaction sequence is reversible, in conflict with experiment.

This situation can be easily remedied by adding Reactions K, L, and M to the mechanism, which creates a dimer on a new layer, which we call Layer n + 1. The resulting structure,  $C_6HH$ , is shown in Figure 3e.  $C_6HH$  is generated when a  $C_6$  species is formed directly in front of or behind (eclipsing) a  $C_6T^*$  species, which has a radical site at the top carbon (Figure 3d),

$$C_6 + C_6 T^* + H^{gas} = C_6 H H + H_2^{gas}. \tag{M}$$

Because  $\Delta G \ll 0$  for Reaction M, it is effectively irreversible (assuming that we have not omitted some other etching reactions of  $C_6HH$  which could convert it back to  $C_5$ ), and  $C_6HH$  ultimately covers half a monolayer. The rate of formation of that half-monolayer would correspond to an effective linear growth rate of around 7 microns/hour. However, since after approximately 100 ms growth is effectively stopped until the trough sites can be filled in, the actual growth rate is limited by whichever process is slower.

#### Trough Mechanism

Although the dimer mechanism including Reactions K through M is relatively fast and irreversible, it accounts for growth only on dimer sites; the trough mechanism adds carbon atoms at the sites which separate the dimers. We take as the starting point for the trough mechanism the structure  $C_6HH$  produced by the dimer mechanism, that is, one dimer already formed on Layer n+1. Because of the large negative values of  $\Delta G$  for Reactions k and l, formation of  $C_6B$  is irreversible via the trough mechanism. Furthermore,  $C_6B$  cannot react back to  $C_6HH$  via the reverse of the dimer mechanism since formation of a dimer-type bond across the trough is not

energetically feasible.  $C_6B$  formation is followed by a rapid reactions analogous to Reactions K through M of the dimer mechanism in which a pair of eclipsed  $C_6B$  species reacts to form a dimer bond on Layer n+1. Thus, the combined dimer/trough mechanism starts with two dimer bonds and creates a new surface containing two dimer bonds, one each from the dimer and trough parts of the mechanism.

There are a couple of approximations implicit in this picture that should be pointed out. First, in order to keep the reaction mechanism manageable we have made an independent sub-unit approximation, assuming that the kinetic and thermodynamic parameters for each dimer-trough pair are independent of the status at neighboring dimer-trough pairs. Second, we note that when all of the dimer-trough pairs have reacted the new surface is again a (100)- $(2\times1)$ :H surface, but it has not been returned to a structure identical to the starting structure because the dimer bonds formed on Layer n+1 are at right angles to those on Layer n. In fact, because of the abcabc... structure of the diamond lattice, Layer n is not reproduced until Layer n+4. However, the structures of each of these layers are congruent—they are merely shifted or rotated. Thus, we assume that the growth rate of each layer between n and n+4 takes place at the same rate.

faster than Reactions d or f, in which the surface growth processes continue. In contrast, the reverse of Reaction s, in which the  $CH_3$  from  $C_6^*M$  desorbs, is an order of magnitude slower than the irreversible formation of  $C_6B$  in Reaction l. This difference is a consequence of the considerably greater steric repulsion in  $C_6HM$  compared to  $C_6^*M$ , which leads to spontaneous  $CH_3$  desorption lifetimes at 1200 K of 100  $\mu$ s and 11 ms for the two species, respectively. As a result, most of the  $C_6B$  which is formed passes through Reaction s rather than Reaction c, even though  $C_6^{**}$  is a relatively high energy species. The hydrogen atom concentration also plays a role, since irreversible incorporation of carbon into the lattice requires abstractions by gas phase H atoms which compete with methyl desorption. We have published previously our predictions for the effect of H atom concentration on growth rates [3, 4], but we are not aware of any experimental data which test them.

#### Discussion

Since a (100)- $(2\times1)$ :H surface contains equal numbers of dimer and trough sites, the dimer and trough mechanisms ultimately contribute equally to growth. However, steric repulsion controls how and when these mechanisms play their roles. The interactions between these mechanisms can be discussed with reference to the drawing in Figure 4, which labels dimer sites as a, c, e, and g, and trough sites as b, d, f, and h.

Growth of Layer n+1 can commence only with the dimer mechanism and not the trough mechanism. This is because spanning a trough giving a hypothetical  $C_5B$ structure would create highly strained bonds and would be unstable because the C-C bonds would have to be too long. Thus, the first reactions are reversible formation of  $C_6$  species on the dimer sites a, c, e, or g followed by the irreversible formation of  $C_6HH$ .  $C_6HH$  sites will not in general exist simultaneously at a and c or at e and g because that would lead to large H-H steric repulsions across the trough. This would shift the reactions

$$C_5M^* \rightleftharpoons C_d^* \rightleftharpoons C_6^*$$

strongly to the left and slow the dimer mechanism. Therefore, once a new dimer bond  $C_6HH$  forms at c and g, for example, reaction at a and e to make another  $C_6HH$  structure there is unlikely. However, the presence of a  $C_6HH$  species at c and g shortens the distance across the trough, which allows troughs b, d, f, and h to be spanned. Thus,  $C_6B$  structures are formed with the trough mechanism, and these react with each other to form additional dimer bonds on Layer n+1. At this point, with the trough hydrogens eliminated, the dimer mechanism rapidly adds carbon at a and e. Thus, growth on the (100)-(2×1):H surface occurs in a coordinated fashion, first up and down rows of (eclipsed) dimers, then up and down adjacent rows of (eclipsed) troughs, then up and down the remaining rows of (eclipsed) dimers.

According to our analysis, the steady state growth rate at dimer sites is considerably faster than at trough sites. Since a complete new layer cannot form until addition has taken place at each trough site, the trough mechanism is rate limiting. This result may provide an explanation for the observation that experimental growth rates can be calculated with the trough mechanism, as seen in Figure 1.

#### **Atomically Smooth Surfaces on Diamond**

In this work we have represented the surface by an ensemble of independent subunits consisting of a pair of dimer bonds next to a pair of troughs, such as sites a, b, e, and f (see Figure 3a). To some extent this representation is adequate. For example, the difference in steric energy between  $C_5$  and  $C_5M$  changes by only around 1 kcal/mole, depending on whether or not a  $C_6HH$  structure is adjacent to the  $C_5$ . Furthermore, the independent sub-unit representation does allow us to predict a certain amount of coordination between subunits. For example, because of the alternating nature of the dimer/trough mechanism, we found that neighboring dimer rows cannot grow until the trough between them has been spanned. However this approach does not account for the relatively smooth surfaces that have sometimes been observed over long ranges on the (100)-(2×1):H surface [28,30,31]. On metals and some other types of crystals, smooth surfaces are the result of loosely bound adatoms diffusing to steps and kinks, which lowers their energy (by increasing their coordination numbers) and leads preferentially to growth at those sites. This process produces fast lateral growth and smooth surfaces. In contrast, it is unlikely that chemically bound hydrocarbon adsorbates would be mobile on a hydrogenated diamond surface [48]. Furthermore, the coordination number of hydrocarbon adsorbates is unaffected by whether they are bound at step or terrace sites. Thus, diffusion of adsorbates to steps and kinks would not provide a mechanism for explaining atomically smooth growth on diamond.

We suggest instead that steric and thermochemical factors can favor growth at step sites over growth on smooth surfaces. For example, we have already shown that growth on atomically smooth (111) surfaces is highly unlikely with a straightforward abstraction-addition mechanism [34]. As we have pointed out above, smooth unreconstructed (100) surfaces may well not exist, but we found previously [3] that methyl radical addition at step sites with (100) character can readily occur because these sites are in general less sterically crowded. Similarly, addition to (110)- or dimer/trough-type sites may be sterically easier at steps than on flat surfaces. If growth intermediates are more stable at step and kink sites, growth would occur preferentially there for the same reason that growth with the trough mechanism occurs preferentially through  $C_6M$  rather than through  $C_6HM$ . The result would then be fast lateral growth leading to smooth surfaces.

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#### REFERENCES

- [1] J. C. Angus and C. C. Hayman, Science 241, 913 (1988).
- [2] S. J. Harris, Applied Physics Letters 56, 2298 (1990).
- [3] S. J. Harris and D. N. Belton, Thin Solid Films 212, 193 (1992).
- [4] D. N. Belton and S. J. Harris, Journal of Chemical Physics 96, 2371 (1992).
- [5] M. Frenklach and H. Wang, Physical Review B 43, 1520 (1991).
- [6] M. Frenklach and K. E. Spear, Journal of Materials Research 3, 133 (1988).
- [7] D. Huang, M. Frenklach, and M. Maroncelli, Journal of Physical Chemistry 92, 6379 (1988).
- [8] M. E. Coltrin and D. S. Dandy, Journal of Applied Physics (submitted).
- [9] W. A. Yarbrough, in *Diamond Optics IV*, edited by A. Feldman and S. Holly (Proc. SPIE, 1991), p. 1534.
- [10] P. Deak, J. Giber, and H. Oechsner, Surface Science 250, 287 (1991).
- [11] S. J. Harris, A. M. Weiner, and Thomas A. Perry, Applied Physics Letters 53, 1605 (1988).
- [12] D. G. Goodwin and G. G. Gavillet, Journal of Applied Physics 68, 6393 (1990).
- [13] C. J. Chu, M. P. D'Evelyn, R. H. Hauge, and J. L. Margrave, Journal of Applied Physics 70, 1695 (1991).
- [14] C. E. Johnson, W. A. Weimer, and F. M. Cerio, Journal of Materials Research 7, 1427 (1992).
- [15] Y. Matsui, H. Yabe, and Y. Hirose, Japanese Journal of Applied Physics 29, 1552 (1990).
- [16] S. J. Harris, A. M. Weiner, and T. A. Perry, Journal of Applied Physics 70, 1385 (1991).
- [17] S. J. Harris and A. M. Weiner, Thin Solid Films 212, 201 (1992).

- [18] L. Schafer, M. Sattler, and C.-P. Klages, "Upscaling of the hot-filament CVD process for deposition of diamond films on large-area substrates", Applied Diamond Conference, August, 1991, Auburn, Alabama, poster.
- [19] W. A. Yarbrough, K. Tankala, and T. DebRoy, Journal of Materials Research 7, 379 (1992).
- [20] D. G. Goodwin, Applied Physics Letters 59, 277 (1991).
- [21] T. G. Owano, D. G. Goodwin, C. H. Kruger, and M. A. Cappelli, Second International Conference on the New Diamond Science and Technology (Washington, DC, 1990), p. 497. Paper 7.2.
- [22] D. G. Goodwin, unpublished.
- [23] K. R. Stalder and R. L. Sharpless, Journal of Applied Physics 68, 6187 (1990).
- [24] Y. Matsui, A. Yuuki, M. Sahara, and Y. Hirose, Japanese Journal of Applied Physics 28, 1718 (1989).
- [25] N. G. Glumac and D. G. Goodwin, Thin Solid Films 212, 122 (1992).
- [26] Y. L. Yang and M. P. D'Evelyn, Journal of the Americal Chemical Society 114, 2796 (1992).
- [27] M. P. Everson and M. A. Tamor, Journal of Vacuum Science and Technology A 9, 1570 (1991).
- [28] L. F. Sutcu, C. J. Chu, M. S. Thompson, R. H. Hauge, J. L. Margrave, and M. P. D'Evelyn, Journal of Applied Physics 71, 5930 (1992).
- [29] V. Baranauskas, M. Fukui, C. R. Rodrigues, and N. Parizotto, Applied Physics Letters 60, 1567 (1992).
- [30] T. Tsuno, T. Imai, Y. Nishibayashi, K. Hamada, and N. Fujimori, Japanese Journal of Applied Physics 30, 1063 (1991).
- [31] H. Sprang, H. G. Busmann, and I. V. Hertel, Second European Conference on Diamond, Diamond-like and related coatings (Nice, France, 1991), p. 443.
- [32] Y. L. Yang and M. P. D'Evelyn, Journal of Vacuum Science and Technology A,

- (1992).
- [33] S. J. Harris and D. N. Belton, Japanese Journal of Applied Physics 30, 2615 (1991).
- [34] S. J. Harris, D. N. Belton, and R. J. Blint, Journal of Applied Physics 70, 2654 (1991).
- [35] W. L. Hsu, Proceedings of the Electrochemistry Society (Electrochemical Society, Pennington, NJ, Pennington, NJ, 1991).
- [36] S. J. Harris and A. M. Weiner, Journal of Applied Physics 67, 6520 (1990).
- [37] F. G. Celii and J. E. Butler, Applied Physics Letters 54, 1031 (1989).
- [38] C. Musgrave, W. A. Goddard, and S. J. Harris, unpublished.
- [39] E. Pearson, T. Takai, T. Halicioglu, and W. A. Tiller, Journal of Crystal Growth 70, 33 (1984).
- [40] J. Tersoff, Physical Review Letters 56, 632 (1986).
- [41] D. W. Brenner, Physical Review B 42, 9458 (1990).
- [42] N. L. Allinger, Journal of the Americal Chemical Society 99, 8127 (1977).
- [43] J.-H. Lii and N. L. Allinger, Journal of the Americal Chemical Society 111, 8551 (1989).
- [44] R. Lee, University of Georgia, Private communication.
- [45] B. J. Garrison, E. J. Dawnkaski, D. Srivastava, and D. W. Brenner, Science 255, 835 (1992).
- [46] D. Huang and M. Frenklach, Journal of Physical Chemistry 96, 1868 (1992).
- [47] E. I. Axelsson, K. Brezinsky, F. L. Dryer, W. J. Pitz, and C. K. Westbrook, Twenty-first Symposium (International) on Combustion (The Combustion Institute, Seattle, WA, 1986), p. 783.
- [48] S. P. Mehandru and Alfred B. Anderson, Journal of Materials Research 5, 2286 (1990).

Table 1

# **DIMER MECHANISM**

REACTION			$\Delta G^a_{1200}$	$k^b$
$A.  C_5 + H^{gas}$	=	$C_5^* + H_2^{gas}$	-14.2	$2.52 \times 10^{14} e^{-7300/RT}$
$B.  C_5^* + H^{gas}$	$\rightleftharpoons$	$C_5$	-59.5	$1.0 \times 10^{13}$
$C.  C_5^* + CH_3^{gas}$	==	$C_5M$	-30.2	$5.0\times10^{12}$
$D. C_5M + H^{gas}$	$\rightleftharpoons$	$C_5M^* + H_2^{gas}$	-16.9	$2.81 \times 10^7 T^2 e^{-7700/RT}$
$E.  C_5 M^* + H^{gas}$		$C_5M$	-57.6	$1.0 \times 10^{13}$
$F.  C_5 M^* + H^{gas}$	==	$C_5^* + CH_3^{gas}$	-27.4	$3.0\times10^{13}$
$G. C_5M^*$		$C_d^*$	+4.3	$1.0 \times 10^{13}$
$H.  C_d^*$	=	$C_6^*$	-21.2	$6.9 \times 10^{12} e^{-8100/RT}$
$I.  C_6^* + H^{gas}$	<b>=</b>	$C_{6}$	-48.5	$1.0 \times 10^{13}$
$J.  C_6 + H^{gas}$	<b>≠</b>	$C_6^* + H_2^{gas}$	-25.2	$1.26 \times 10^{14} e^{-7300/RT}$
V.C. C. III.		C The . 11 gas	00.0	0.0106/T2 = 5000/RT
$K.^{c}$ $C_6 + H^{gas}$		•	-22.9	$9.0\times10^6T^2e^{-5000/RT}$
$L.^{c}$ $C_{6}T^{*} + H^{gas}$	=	$C_6$	-50.8	$1.0\times10^{13}$
$\underline{M.^c  C_6T^* + C_6 + H^{gas}}$	=	$C_6HH + H_2^{gas}$	-61.1	$1.8 \times 10^7 T^2 e^{-5000/RT}$

- a. units are kcal/mole
- b. units are cm<sup>3</sup>, moles, seconds
- c. Analogous reactions can be written for  $C_6^*$ .

Table 2

# TROUGH MECHANISM

REACTION			$\Delta G^{1200}$	
$\frac{a. C_6 H H + H^{gas}}{a. C_6 H H + H^{gas}}$		C U+ 1 Ugas		$\frac{1.3 \times 10^{14} e^{-7300/RT}}{1.3 \times 10^{14} e^{-7300/RT}}$
	=	$C_6H^* + H_2^{gas}$	-16.1	
$b. C_6H^* + H^{gas}$	=	$C_6HH$	-57.6	$1.0\times10^{13}$
$c. C_6H^* + CH_3^{gas}$	==	$C_6HM$	-20.6	$5.0\times10^{12}$
$d. C_6 HM + H^{gas}$	==	$C_6^*M + H_2^{gas}$	-30.3	$1.3 \times 10^{14} e^{-7300/RT}$
$e. C_6^*M + H^{gas}$	$\rightleftharpoons$	$C_6HM$	-64.0	$1.0 \times 10^{13}$
$f. C_6 HM + H^{gas}$	=	$C_6HM^*+H_2^{gas}$	-19.1	$2.8\times10^{7}T^{2}e^{-7700/RT}$
$g. C_6 H M^* + H^{gas}$	=	$C_6HM$	-54.6	$1.0\times10^{13}$
$h. C_6 H M^*$	==	$C_6^*M$	-11.2	$1.0\times10^8$
$i. C_6 H M^* + H^{gas}$	<b>=</b>	$C_6H^*+CH_3^{gas}$	-34.0	$3.0 \times 10^{13}$
$k. C_6 H M^* + H^{gas}$	<del>==</del>	$C_6B + H_2^{gas}$	-67.3	$1.3 \times 10^{14} e^{-7300/RT}$
$l. C_6^*M + H^{gas}$	===	$C_6B + H_2^{gas}$	-56.1	$2.8 \times 10^7 T^2 e^{-7700/RT}$
$m. C_6 H H + H^{gas}$	=	$C_6^*H + H_2^{gas}$	-22.3	$1.3 \times 10^{14} e^{-7300/RT}$
$n. C_6^*H + H^{gas}$	=	$C_6HH$	-51.4	$1.0\times10^{13}$
$o. C_6 H^* + H^{gas}$	==	$C_6^{**} + H_2^{gas}$	-18.7	$1.3 \times 10^{14} e^{-7300/RT}$
$p. C_6^{**} + H^{gas}$	==	$C_6H^*$	-55.0	$1.0 \times 10^{13}$
$q. C_6^*H + H^{gas}$	⇌	$C_6^{**} + H_2^{gas}$	-12.5	$4.5 \times 10^6 T^2 e^{-5000/RT}$
$r. C_6^{**} + H^{gas}$	==	$C_6^*H$	-61.2	$1.0\times10^{13}$
s. $C_6^{**} + CH_3^{gas}$	==	$C_6^*M$	-32.2	$5.0\times10^{12}$
$t. C_6 H^*$	=	$C_6^*H$	-6.2	$1.0 \times 10^{8}$

Table 3

THERMOCHEMISTRY FOR DIMER MECHANISM

SPECIES	H a	$S^a$	$G^{a,b}$	$n_s$
	kcal/mole	cal/mole-Kelvin	kcal/mole	
$\overline{C_5}$	0.0	0.0	0.0	2
$C_5^*$	+44.0	-0.1	+44.1	1
$C_5M$	9.1	+20.5	-15.4	3
$C_5M^*$	+51.3	+20.4	+26.8	2
$C_d^*$	+56.2	+20.9	+31.1	1
$C_6^*$	+27.9	+15.0	+9.9	1
$C_6$	-5.8	+14.5	-23.2	2
$C_6T^*$	+32.8	+17.2	+12.2	1
$H^{gas}$	56.6	34.3	+15.4	
$H_2^{gas}$	6.4	41.1	-42.9	
$CH_3^{gas}$	46.1	62.8	-29.3	

a. Values for H and S and G are for 1200 K. Values for all surface species referenced to  $C_5$ .

Table 4

# THERMOCHEMISTRY FOR TROUGH MECHANISM

SPECIES	H <sup>a</sup>	$S^a$	$G^a$	$\overline{n_s}$
	kcal/mole	cal/mole-Kelvin	kcal/mole	
$\overline{C_6 H H}$	+11.4	+21.0	-13.8	1
$C_6H^*$	+51.7	+19.5	+28.4	1
$C_6^*H$	+46.1	+19.9	+22.2	1
$C_6^{**}$	+90.0	+18.4	+68.0	1
$C_6HM$	+26.9	+40.3	-21.5	3
$C_6HM^*$	+65.8	+40.1	+17.7	1
$C_6^*M$	+53.3	+38.9	+6.5	3
$C_6B$	+40.9	+26.9	+8.7	1

a. Values for H and S and G are for 1200 K. Values for all surface species referenced to  $C_5$ .

## Captions

- 1. Comparison of measured growth rates with growth rates predicted from numerical simulations [20-22] using the trough mechanism [2]. The environments simulated were an oxygen-acetylene flame [24] (solid squares), a 220 torr DC arcjet [23] (open circle), an atmospheric-pressure RF torch [21] (open squares), a 40 Torr acetylene-oxygen flat flame [25] (solid triangle), and a hot-filament system [22] (solid circle). The calculations use the parameters given in the paper proposing the BCN mechanism [2] with the exception of the rate constant for H atom recombination at radical sites. This value was adjusted from 10<sup>14</sup> to 5 × 10<sup>13</sup> cm<sup>3</sup>/mole-s because the former value implies a recombination rate equal to twice the collision rate.
- 2. The diamond slab used as the model compound for calculating steric repulsion energies.
- 3. Surface structures considered in this work. The letters A, B, C, and D represent adducts on the crystal slab.

(a) 
$$C_5$$
  $(A = H)$ ;  $C_5^*$   $(A = ^*)$ ;  $C_5M$   $(A = CH_3)$ ;  $C_5M^*$   $(A = CH_2^*)$ .

- (b)  $C_d^*$ .
- (c)  $C_6^*$   $(B = ^*); C_6$  (B = H).
- (d)  $C_6$  eclipsing a  $C_6T^*$ .

(e) 
$$C_6HH$$
 ( $C = H, D = H$ );  $C_6H^*$  ( $C = H, D = *$ );

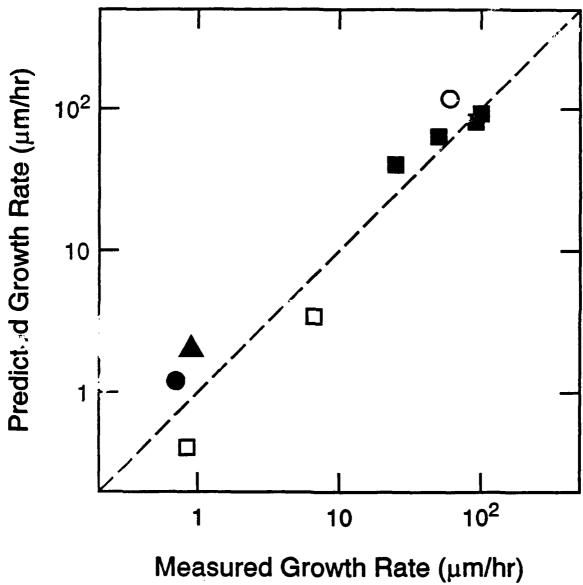
$$C_6HM$$
  $(C = H, D = CH_3); C_6^*M$   $(C = ^*, D = CH_3);$ 

$$C_6HM^*$$
  $(C=H,\,D=CH_2^*);\,C_6^{**}$   $(C=^*,\,D=^*);$ 

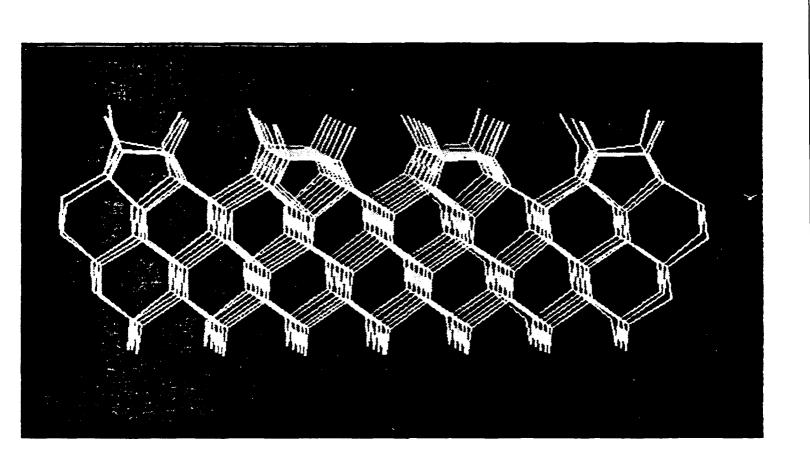
$$C_6H^*H\ (C=^*,\, D=H).$$

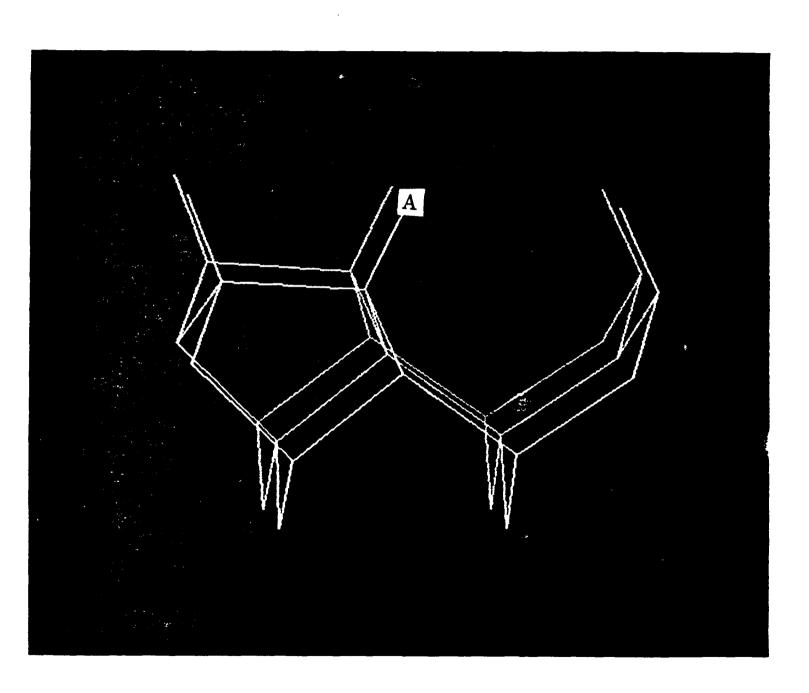
(f)  $C_6B$ .

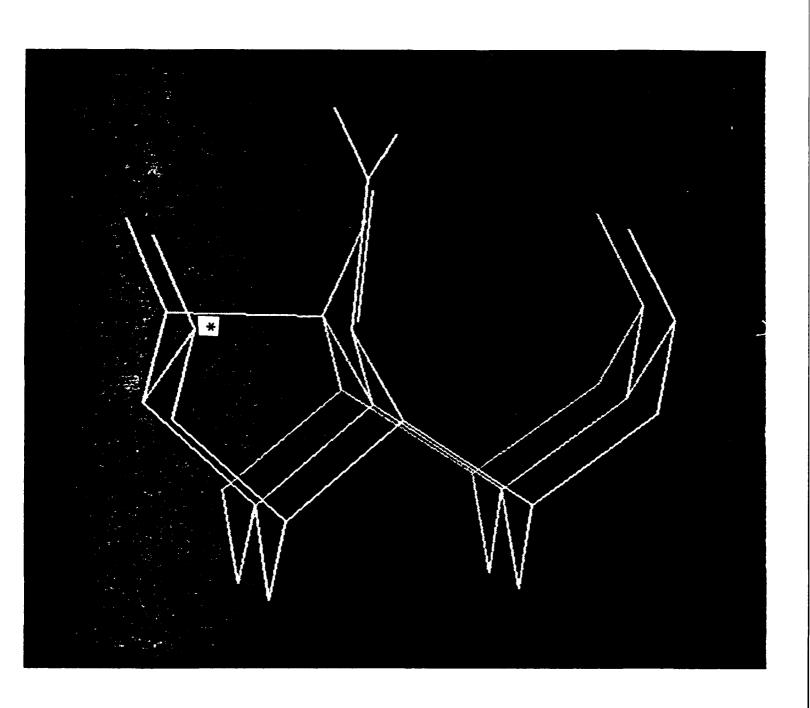
4. Structure of a portion of the (100)- $(2\times1)$ :H surface. Positions labeled a, c, e, and g are sites for addition with the dimer mechanism positions labeled b, d, f, and h are sites for addition with the trough mechanism.

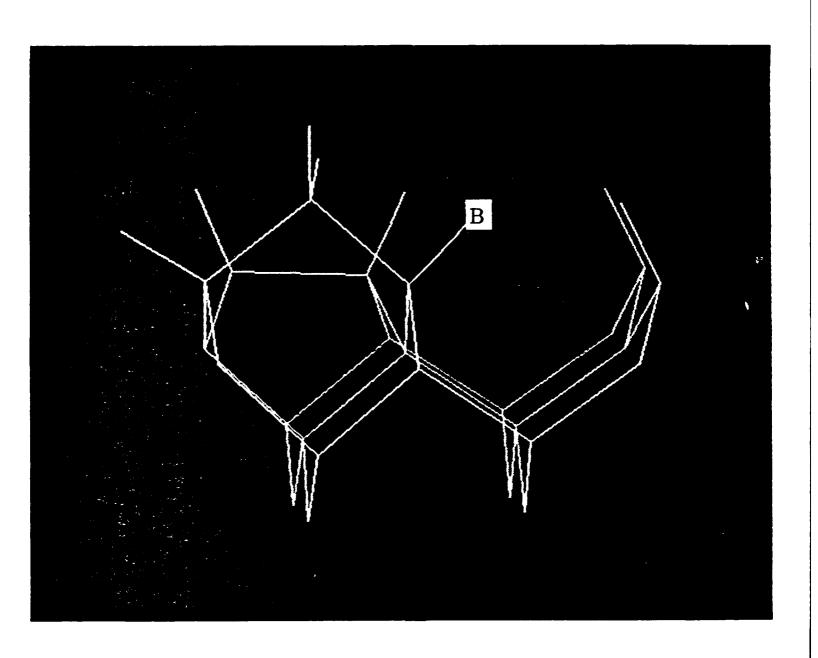


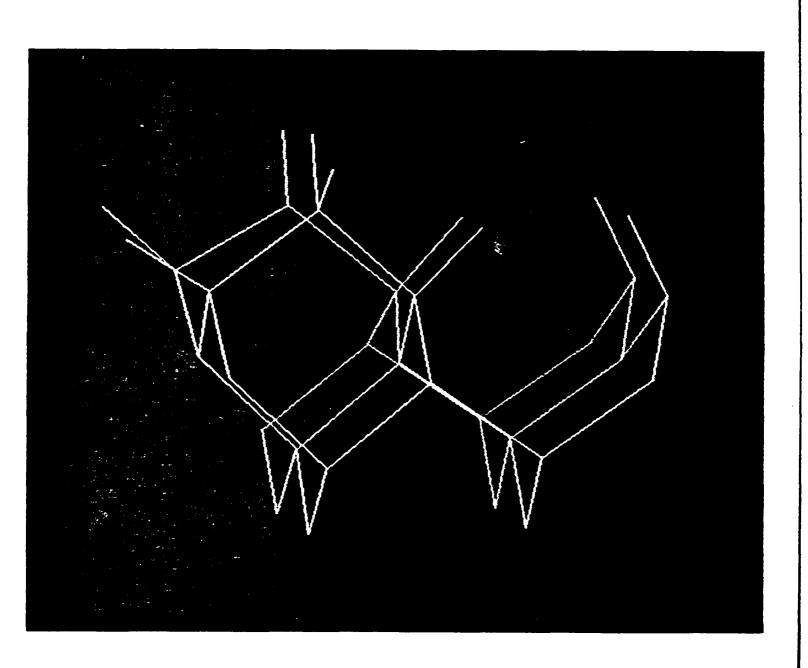
moderated diowth rate (μπιππ)

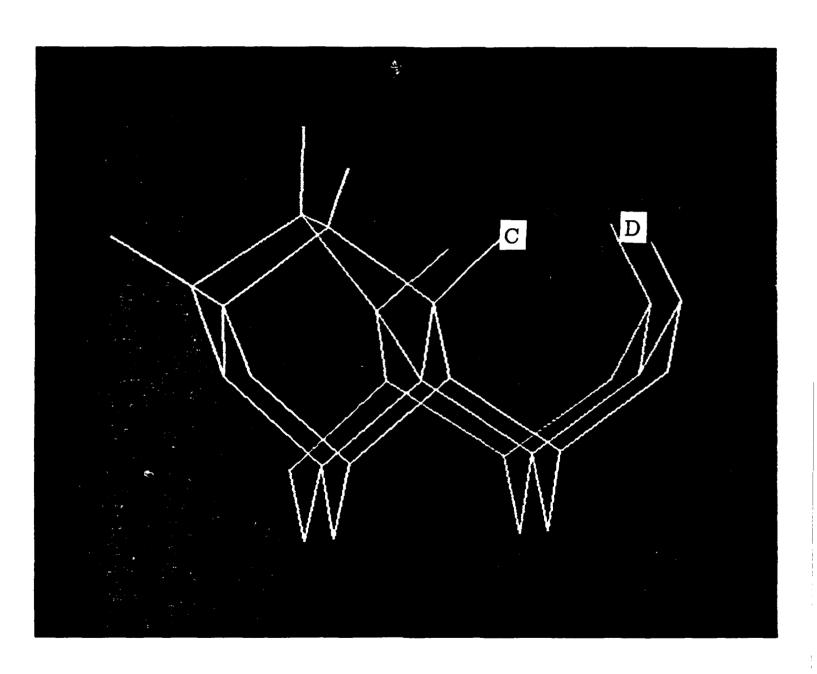


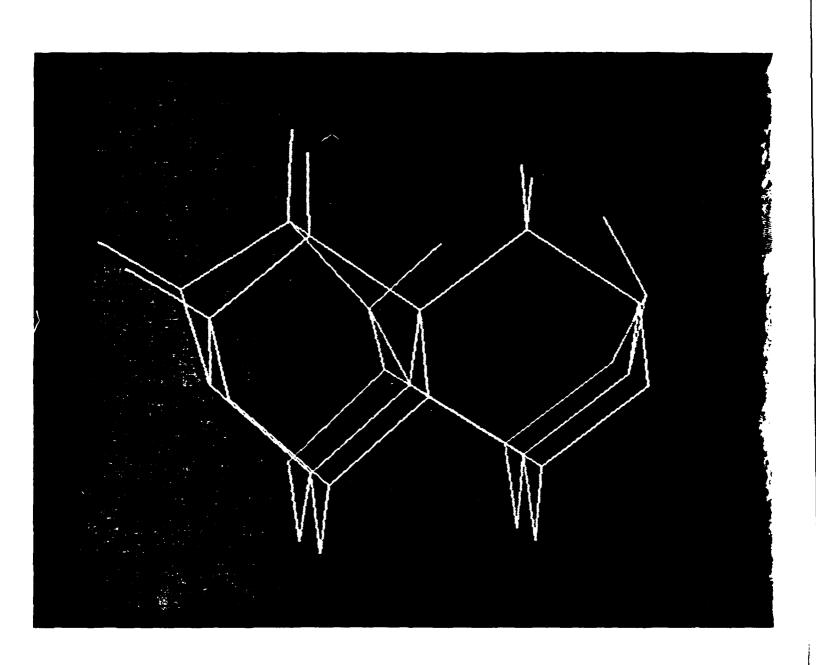


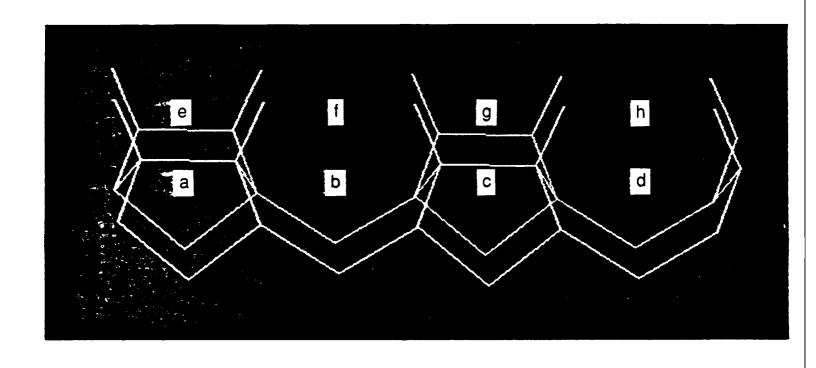












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